

# **amateur radio**

Vol. 36, No. 12

**DECEMBER 1968**

Registered at G.P.O., Melbourne, for  
transmission by post as a periodical

# Merry Christmas and Happy New Year to all our Clients

## FIXED CONDENSERS

125 Volt Ratings:

10, 15, 16, 22, 27, 33, 39, 47, 50, 60, 62, 100, 120, 150, 220, 270, 330, 390, 425, 470, 500 pF. all 15c ea.

0.01	uF.	160V.	120	0.0018	uF.	600V.	18c
0.01		125V.	250	0.0022		800V.	18c
0.012		125V.	13c	0.0022		600V.	18c
0.012		400V.	12c	0.0027		400V.	17c
0.012		800V.	12c	0.0027		600V.	18c
0.015		125V.	13c	0.0033		400V.	12c
0.015		600V.	18c	0.0033		600V.	14c
0.018		600V.	22c	0.0039		400V.	12c
0.021		600V.	25c	0.0047		800V.	18c
0.022		400V.	14c	0.0047		400V.	15c
0.022		400V.	24c	0.0047		600V.	22c
0.027		160V.	14c	0.0056		400V.	15c
0.027		400V.	15c	0.0056		600V.	13c
0.027		600V.	22c	0.0068		400V.	15c
0.033		125V.	14c	0.0068		600V.	15c
0.033		125V.	15c	0.01		125V.	15c
0.033		600V.	22c	0.1		400V.	18c
0.039		125V.	14c	0.1		600V.	27c
0.039		600V.	25c	0.2		400V.	20c
0.039		600V.	28c	0.5		400V.	20c
0.047		125V.	14c	0.12		125V.	25c
0.047		400V.	14c	0.12		800V.	20c
0.047		600V.	14c	0.15		125V.	15c
0.056		125V.	14c	0.15		400V.	15c
0.056		400V.	14c	0.15		600V.	29c
0.056		600V.	18c	0.18		125V.	17c
0.056		125V.	13c	0.18		400V.	17c
0.056		400V.	14c	0.22		125V.	15c
0.056		600V.	18c	0.22		400V.	22c
0.056		600V.	25c	0.22		600V.	24c
0.056		400V.	22c	0.27		125V.	22c
0.056		600V.	28c	0.27		400V.	25c
0.061		125V.	15c	0.27		600V.	28c
0.061		400V.	15c	0.33		125V.	25c
0.061		600V.	18c	0.33		400V.	28c
0.061		5KV.	45c	0.39		160V.	22c
0.061		5KV.	45c	0.39		400V.	40c
0.061		5KV.	45c	0.47		125V.	28c
0.061		5KV.	45c	0.47		400V.	35c
0.061		5KV.	45c	0.47		600V.	40c
0.061		5KV.	45c	0.88		125V.	35c

## MULTIMER, Model OL-64

20,000 ohms per volt d.c., 8,000 ohms per volt a.c.

Specifications:

D.C. volts: 0-0.1, 1, 10, 50, 250, 500, 1,000, 5,000.  
A.C. volts: 0-15, 50, 250, 1,000.  
D.C. current: 0-0.1, 1, 50, 500 mA.; 10 A.  
Resistance: 0-5, 500 ohms; 5, 500 megohms.  
Decibels: Minus 20 to plus 22 db., plus 20 to plus 30 db.  
Capacitance: 250 pF. to 0.02 uF.  
Inductance: 0-5000 H.  
Load current: 0-0.05, 0.6, 60 mA.  
Cell contained batteries: 22.5V. (BL-015) x 1, 1.5V. (UM3) x 2.  
Size and weight: 6 x 4-1/5 x 2 in. 650 g.  
Meter movement full, sensitivity: 30 uA., F.S.D.  
Price \$19.73, postage 25c.

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Stand to suit

\$2.90 extra.

Packing and Postage 25c.

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1/2 watt: 8c ea. or 58.00 per 100

1 watt: 70c ea. or 57.00 per 100

When ordering 100 or over, minimum quantity of 10 of each selected type.

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20,000 ohms per volt d.c., 10,000 ohms per volt a.c.

Specifications:

D.C. volts: 0-0.5, 25, 250, 500, 2500.  
A.C. volts: 0-10, 50, 250, 500.  
D.C. current: 0-50 mA.  
Resistance: 0-100 ohms.  
Ohms: 0-5 meg.  
Capacity: 0.01 - 0.3 uF. (at A.C. 50 Hz.)  
0.0001-0.01 uF. (at A.C. 250V.).  
Decibels: Minus 20 to plus 22 db.  
Output range: 0-10, 50, 100, 500, 1000.  
Battery used: UM3 1.5V., 1-piece.  
Dimensions: 3 1/2 x 4 1/2 x 1 1/2 inch.  
Price \$11.25, inc. tax, Post free.  
Complete with internal battery, testing leads, prods.



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## BARGAINS!!

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NE2 Neons ... 90v. 30c; 240v. 50c  
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" " S0515 ... 31.50 ea.  
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		3 1/2 INCH REELS		
600 Feet	—	Mylar Base	...	\$1.85
		4 INCH REELS		
400 Feet	—	Acetate Base	...	\$1.40
		5 INCH REELS		
600 Feet	—	Acetate Base	...	\$1.45
900 Feet	—	Acetate Base	...	\$2.30
900 Feet	—	Mylar Base	...	\$3.00
1200 Feet	—	Mylar Base	...	\$3.80
1800 Feet	—	Mylar Base	...	\$5.75
		5 1/2 INCH REELS		
900 Feet	—	Acetate Base	...	\$2.45
1200 Feet	—	Acetate Base	...	\$3.40
1200 Feet	—	Mylar Base	...	\$3.75
1800 Feet	—	Tensilised Mylar Base	...	\$4.75
		7 INCH REELS		
1200 Feet	—	Acetate Base	...	\$3.00
1200 Feet	—	Mylar Base	...	\$3.75
1800 Feet	—	Acetate Base	...	\$4.50
1800 Feet	—	Mylar Base	...	\$5.00
2400 Feet	—	Mylar Base	...	\$6.25
3000 Feet	—	Mylar Base	...	\$9.75
		EMPTY REELS		
3 inch	...	25c	5 inch	40c
3 1/2 inch	...	30c	5 1/2 inch	55c
4 inch	...	35c	7 inch	90c
Postage 20c.				

## POWER TRANSFORMERS

Type	H.T. Sec. Volts	Max. D.C. mA.	HEATER DOUBLER TYPES		Price
			Heater Windings V. A.	Rectifier V. A.	
PT2062	115	90	6.3CT 2.25		\$10.80
PT2063	taps 105, 135	100	6.3CT 2.25		\$13.40
PT2067	taps 120, 125	100	6.3CT 4		\$13.00
PT2064	taps 110, 125	125	6.3 2.25		\$12.30
PT2065	taps 120, 125	125	6.3CT 2.25		\$12.30
PT2068	115	150	6.3CT 6		\$13.60
PT5324	taps 105, 125	150	6.3CT 3		\$12.20
PT2068	taps 110, 104	100	6.3CT 3		\$13.70
PT2068	taps 185, 175	200	6.3 4		\$20.00
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## FULL WAVE TYPES—VALVE RECTIFIER

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PT1951	180-0-180	40	6.3 2		\$6.70
PT1940	225-0-225	60	6.3 2		\$8.50
PT1993	225-0-225	50	6.3 2		\$5.70
PT1941	285-0-285	80	6.3 2		\$9.00

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# amateur radio

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53.855 Mc. a.m. (53.550 Mc. f.m.  
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7145 Kc. a.m. 143.500 Mc. a.m.  
53.632 Mc. a.m.

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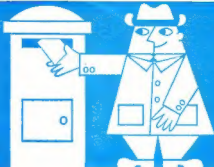
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## FEDERAL COMMENT

### *The Year in Review*

As mentioned in last month's issue, the development of Region III activities has probably been the highlight of the year. Since the Federal President's comment we have now received agreement to the Region III interim constitution from the Philippines. In a letter from Emilio DUIEA, a further amendment is made to the status of the Amateur Radio organisation in that country, and we can do no better than quote the relevant section:

"In view of the establishment of a new organisation of Radio Amateurs in the Philippines, viz. 'Philippine Amateur Radio Service Inc.' (P.A.R.S.), the other Societies—P.A.R.A. and P.A.R.L.—are now only chapters of P.A.R.S. The P.A.R.S. will now replace P.A.R.A. for purposes of membership with the I.A.R.U., and is the only organisation, of which I am the President, recognised by the Philippine Government".

We congratulate Emilio and note with interest his last point.

Our domestic scene can be viewed in the light of progress, too, and arising from the Federal Convention discussions last Easter, a committee was formed to investigate all aspects of "A.R." By the time this is read, copies of the report should be in all Divisions and you are urged to read it and become informed of the many problems confronting the Editor and his Committee.

Nearly all matters arising from this Convention have been dealt with, although a proposal that some sort of code proficiency test be run is still being worked out in conjunction with the VK7 Division.

We also saw the very liberal provisions by the Postmaster-General's Department in reply to our request to use v.h.f. repeaters, and in the subsequent enthusiasm resulting in a conference at Wodonga, many plans have been made for operational repeaters. This Institute felt that the frequencies and modes proposed were worthy of adoption as policy and they are being considered by Divisions. There does appear, however, to be some aspects at variance with the Tasmanian group's thoughts on the matter and it is hoped that the VK2 repeater secretariat can assist in providing a solution.

Whilst speaking of v.h.f., we would refer you to the published statement, shown elsewhere in this issue, from the I.T.U. Administrative Council. Any comment from us at this stage would be pure speculation, but you should be aware that we are being kept informed of all and any developments. When a more specific agenda is available—perhaps during the middle of this coming year—we will know a little more, and can form a more specific judgment. Whilst our Amateur bands 144 Mc. and above are slotted into the part of the spectrum under review, the preparations to try and counter any inroads by other services are no less stringent than they would be for h.f. bands.

Your Federal Councillor and Division will be asking you for reports on v.h.f. activities and achievements, and we suggest that this information be provided as soon as possible. The significance of this information, or the lack of it, will be obvious.

It is interesting to note that in this country, the number of civil radio

communication stations between 143 and 174 Mc. amounted to 14,500 over twelve months ago. In nine months, the total number of stations in Australia increased from 93,000 to 102,000—so the commercial and civil users have their problems too.

Before leaving you with thoughts of holidays and/or the work to be done around the house, we should mention that you could find time perhaps to suggest ways of improving the national society that represents you, viz. the W.I.A., or the conditions under which we are allowed to operate.

Next Easter, the Federal Convention may be held in Canberra, but no matter where, all Federal Councillors will meet to consider and review past policies, up-date them if necessary, and introduce new ones.

Your suggestions are valued and your Division will be eager to consider all proposals put before it, no matter if it concerns DX, contests, regulations, finance or administration—so while dangle that line or contemplating the beauty of your favourite holiday retreat, why not slip in the thought to do something positive when you return to civilisation?

In the meantime, our best wishes for a pleasant and relaxing Christmas season, with a prosperous 1969 in the offing. With 73 from Federal Councillors: Pierce VK2APQ, Deanne VK-3TX, David VK4DP, Geoff VK3TY, Neil VK6ZDK, Ted VK7EJ, and your Federal Executive: John VK3OR, Michael VK3KI, Peter VK3IZ, David VK-3QV, George VK3VX, Alf VK3IE, and Kevin VK3ARD.

## A TRANSVERTER FOR 21 OR 28 Mc.

AL RECKNER.\* VK5EK

THIS article is written in response to many requests received over the air. I was hesitant to describe this device in "A.R." as several of the parts used are not available "over the counter". This must not, therefore, be regarded as a detailed constructional article, but merely a description of a unit which works very well and from which erstwhile constructors may obtain some hints.

Many owners of three-band transceivers would like to be able to operate on the 21 and 28 Mc. bands, especially at this time of the sunspot cycle. Although this unit was built for 28 Mc. the design is amenable to either or both bands, and probably performs better on those bands than a five-band transceiver.

The circuit consists of a conventional crystal-controlled converter, which converts the 28 Mc. signals to 3.5 Mc. using the three-band transceiver as a tuneable i.f. On transmit, the full output of the transceiver is dissipated in a suitable resistive load, except for a small amount which is fed to a high level mixer. Output from the crystal oscillator in the converter is also fed to this mixer and the sum of these two input frequencies is used to drive the final. The crystal oscillator is on 25,000 Mc. for 28 Mc. we use the sum  $(25 + 2.5 = 28.5)$  and for 31 Mc. we use the difference  $(25 - 3.5 = 21.5)$ ; on this band the tuneable i.f. tunes backwards.

Referring to the circuit; the receiving converter is quite conventional, and almost anything will work here. You already have a 28 Mc. converter built up on a fairly small chassis, then that could be used by mounting it as a sub-chassis on the main chassis. This is what I have done. The i.f. would need to be correct, of course. Careful layout and shielding will pay off with the 6AK5 r.f. amplifier, as these tubes tend to be unstable. Use another type if you like, but keep the noise figure in mind. Almost any sharp cut-off miniature valve would be okay. The resistive anode load in the mixer is easy, and works well. The crystal oscillator is conventional, its h.t. feed point is about 20% up the coil from the crystal end.

People who are supposed to know, throw up their hands in horror at the idea of high-level mixers, but this one works well and is perfectly stable by reason of the low impedance of the grid circuit. I actually used a 5B/254M, but as these are probably unprocureable, I have shown an 807, although a physically smaller tube would be nicer, perhaps a 6146 or a 2E26. Similarly, the 50 ohm, 100 watt resistor will dissipate the output of the transmitter may be heated and, if it should, of course, be more or less non-reactive. The 6AM6 buffer-amplifier between the crystal oscillator and the mixer may be unnecessary, but is probably a wise

precaution. Almost any tube of the 6AM6 type could be used.

The plate circuit of the mixer is a little unusual, it is the so called "series tuned" circuit. This was chosen so that a conveniently small value of neutralising capacity is required. The value of the mixer plate tuning capacitor should be such that when at resonance, its capacity should equal the total of the input capacity of the two final tubes plus the output capacity of the mixer. One way to do this is to short out the tuning condenser and adjust the coil so that it resonates at 0.7 of the required frequency, then remove the short and adjust the condenser to resonance at signal frequency (about 30 pF.). The neutralising capacitor is a piece of brass about 1" square, placed near the two final tubes.

The final tubes are operating in class AB1, and are not in passive grid. They have a very short grid base and consequently stability can be a problem. Neutralising is critical and parasitic suppressors should be in the plate leads and screen leads (I forgot them in the circuit). It would be a good idea to shield the input circuit and the mixer

tube should lie on its side under the chassis.

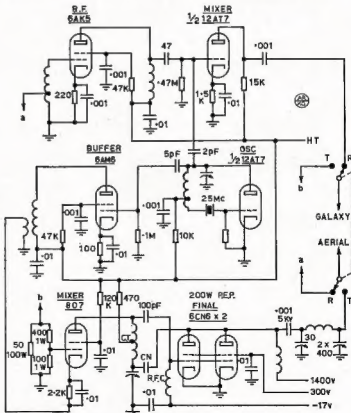
There is adequate drive for the final on 28 Mc., but this may not be so if the final used tubes with a longer grid-base (i.e. 807s or 6146s). A home-made solenoid type r.f. choke is used in the final and is quite okay.

Power supplies are left to the individual, with the thought that a.s.b. amplifiers do not need regulated supplies. I am quite happy with "well regulated supplies". The first implies a horrible concoction of regulator tubes, reference diodes, etc., whilst the second merely means low internal resistance and no series resistance. H.t. may be left on the converter all the time and switched on to the 807 and the final during transmit. Plate voltage can be left on the final all the time and the screen switched. I use a ceramic water switch for the r.f. circuitry, although this does not permit push-to-talk. You could probably use a relay if you had a suitable one.

If I was to build this unit again, I would probably use a low level mixer, say a 12BY7, and then an amplifier,

(Continued on Page 15)

(Continued on Page 15)



# A TRANSVERTER FOR 21 OR 28 Mc/s



# PROJECT—SOLID STATE TRANSCEIVER

## PART TWO

H. L. HEPBURN,\* VK3AFQ, and K. C. NISBET,† VK3AKK

In this second part of the series of articles on a modularised transceiver, it is proposed to deal with the receiver "front-end" and the injection oscillator chain which is common to both receiver and transmitter.

### RECEIVER FRONT-END

Reference to Fig. 1 in the November 1968 issue of "A.R." (included here for convenience of readers) shows that the front end of the receiver consists of Function 1 (receiver r.f. amplifier) and Function 2 (receiver mixer).

Fig. 5 in this article gives the circuit diagram for these functions, while Table 2 lists coil data for the usual h.f. Amateur bands.

Before proceeding with a detailed description of the circuit a general comment must be made.

One of the biggest problems involved in the design of multiband equipment, no matter whether receiver, transmitter or transceiver, is not an electrical one. In the authors' view the problem is mechanical—the physical layout of components associated with the conventional multi-wafer band switch. If, say, a four-band device is required, it is necessary right at the start of building to make provision for the correct number of switch wafers, coil forms, etc., to be in the right position to give minimum lead length. In all probability too, it is necessary to fit metal screens between the various sections. If, later, you want to add a band you are stuck with the original layout and metalwork and can only achieve your objective by recourse to extensive surgery.

In attempting—as this series of articles does—to present a completely flexible design—the need rigidly to fix the physical layout beforehand could not be tolerated. To a very large degree the problem has been overcome by eliminating the need for a complex switch.

The band switch for the whole receiver has been reduced to a single bank selecting the appropriate antenna coil coupling link (L1, Fig. 5) and the 10V. feed rail to each front-end board. This switch bank is physically removed from the boards and connected thereto by co-ax. The outputs of all boards are connected in parallel and are not switched at all.

To eliminate completely any slight puzzlement that may have been caused by reference to front-end boards in the plural, let it be emphasised that there is one complete set of semiconductors and coils for each band covered.

Whilst it is admitted that the approach used is slightly more expensive than the conventional one, it is the only one, in the writers' view, that could be used if the completely flexible modular principle was to be upheld.

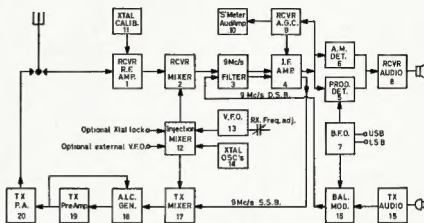


FIG. 1—TRANSISTOR 4 BAND TRANSCEIVER—BLOCK DIAGRAM.

	L1 Input	L2, 3, 4, 5 RF/Mixer Tuned	L7, L8 Oscillator Input	C1, C2 C3, C4	C5, C6	C7	R* RF Source
Band	Link	Circuits	Filters	pF.	pF.	pF.	Resistor
160	10t, 39g.	80t, 39g.	38t, 28g.	470	47	470	Nil
80	10t, 39g.	50t, 39g.	30t, 28g.	150	47	470	Nil
40	7t, 28g.	34t, 28g.	25t, 28g.	150	47	470	Nil
20	7t, 28g.	34t, 28g.	34t, 28g.	33	100	1000	Nil
15	5t, 28g.	20t, 28g.	20t, 28g.	33	47	470	10.0K
10	5t, 24g.	16t, 24g.	25t, 28g.	33	22	220	3.9K.

TABLE 2.—RECEIVER FRONT-END COIL DATA

Notes on Table 2 and Figure 5:—

1. L6 is 38 turns of 28 gauge B. & S.
2. All coils close wound on Neosid Type 722/1 bakelite coil formers.
3. All coils use Neosid F29 tuning slugs.
4. L2/3, L4/5, and L7/8 are mounted 15/32 inch apart to form band pass coupled pairs.
5. L1, the antenna coupling link is close wound over the earthy end of L2.
6. All coils are wound with specified gauge of B. & S.

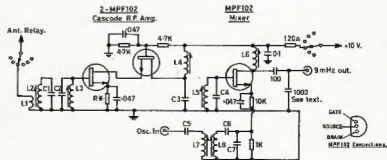


FIG. 5—4 BAND TRANSISTOR TRANSCEIVER—RX. FRONT END.

\* 4 Elizabeth Street, East Brighton, Vic., 3187.  
† 25 Thames Avenue, Springvale, Vic., 3171.

Each front-end printed circuit board is "wired" for two bands so that the four bands as designed uses two p.c.b.s. It is possible to extend the coverage of the unit up to eight bands if desired simply by adding further boards. No mechanical alterations are needed.

The circuitry for each band is shown in Fig. 5.

A fixed tuned, mutually coupled, pair of coils (L2/L3) feeds the gate of the "bottom" half of a cascade of r.f. amplifier using Motorola MPF102 single gate FETs. The source resistor marked \* on the diagram has the primary purpose of keeping the gain constant from band to band. For 160/80/40/20 metres, it is not needed at all.

The gate of the "top" half of the cascade is maintained at half rail potential by the two 4.7K resistors and earthed for r.f. by the 0.047 uF. capacitor.

The r.f. drain coil (L4) is mutually coupled to the mixer gate coil (L5) and proper adjustment of these and the r.f. amplifier coils enables the correct band pass to be achieved.

C5/L7 forms a series tuned circuit on the required injection frequency which is mutually coupled to L8. This latter coil is parallel tuned by the combination of C6 and C7 in series. The low impedance output required by the source method of injection into the mixer is obtained from the junction of C6 and C7.

The reason for the inclusion of L7/L8 is to ensure a pure injection waveform. This is covered more thoroughly in the section following.

The mixer proper is a third MPF102 with a 9 Mc. tuned circuit in the drain. This coil (L6) is tuned by the series combination of the 100 pF. and 1,000 pF. capacitors. Output at low impedance is taken from the junction of the two capacitors. Note that the 1,000 pF. is only needed on the first board made.

Since all board outputs are in parallel, this single 1,000 pF. will effectively be in series with the 100 pF. capacitors on the individual boards. It is of course necessary to re-peak the various L6s when adding more bands because there is some slight interaction between them.

A.g.c. is applied by varying the d.c. applied to the h.t. rail. The method of deriving a supply voltage which varies inversely with signal will be discussed in a later article. Provision is also made for a manual r.f. gain control by the same method of varying the h.t. rail.

## INJECTION OSCILLATOR CHAIN

The three component parts of the oscillator chain are the functions marked 12, 13 and 14 in Fig. 1. They are detailed in this article in Figs. 6, 7 and 8 with the coil data being given by Tables 3, 4 and 5 respectively.

In general, the higher the operating frequency of the v.f.o., the simpler it is to prevent spurious responses. However, there are some obvious difficulties in constructing a really stable v.f.o. at frequencies in the 40-50 Mc. region and, after considerable experiment, the method adopted has been to operate the v.f.o. on 10-10.5 Mc., heterodyne this with a fixed crystal oscillator to

56-56.5 Mc. and then heterodyne down to the required injection frequency with a series of high frequency crystal oscillators.

With a fixed i.f. of 9 Mc. the injection frequencies needed for the various Amateur bands (and the heterodyne crystal frequencies needed to come down from 56-56.5 Mc.) are given in Table 6. Note that in all cases the b.f.o. operates on the u.s.b. crystal and that the correct sideband for the band in use is automatically selected if the specified heterodyne crystals are used. The "other" sideband is available by using the l.s.b. crystal in the b.f.o.

Note, too, that since the same injection frequency is used for both transmit and receive, there can be no offset. If the receiver is tuned to a signal on any band the transmitter comes up on exactly the same frequency and sideband. In many cases, such as participation in round tables, this may be a disadvantage and provision is made for

a received frequency offset facility. This will be described later in the series.

The apparent complexity of the injection train needs comment. However, closer scrutiny will show that there are only a couple of additional stages over the complement of stages normally found in a transceiver. The v.f.o. and crystal heterodyning stages and their associated mixers are common to all current designs. The one vital addition is the 46 Mc. oscillator and its mixer in the v.f.o. generator. This takes the virtual output of the v.f.o. up to 56-56.5 Mc. The reason for this can be summed up in one word... "birdies".

Rather than plough through the mathematics involved, a description of a practical test may be simpler.

The writers carried out a series of tests on four popular commercial sideband rigs and one very good "home brew" job. The test was simple and was as follows:

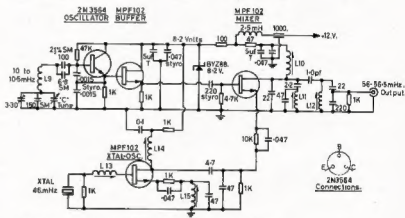


FIG. 5-4 BAND TRANSISTOR TRANSCEIVER - VFO GENERATOR

Coil	Freq. Mc.	Turns	Wire Gauge B. & S.
L9	10-10.5	22	20 approx.
L10	56-56.5	12	20
L11	46 (trap)	12	20
L12	56-56.5	12	20
L13	—	10	28
L14	46	20	28
L15	30-32 approx.	15	28

TABLE 3.—VFO GENERATOR COIL DATA

Notes on Table 3 and Figure 6:—

- All coils close wound on Neosid Type 722/1 bakelite formers.
- L9 is "J" diameter, 16 turns per inch, "Willis" air wound inductance No. 3-16 (or B. & W. No. 3011), obtainable from William Willis and Co. Pty. Ltd., 430 Elizabeth St., Melbourne.
- The tuning condenser  $C_{TOS}$  is an Eddystone No. 585 4.5 to 91 pF. single section variable.

The receiver under test was set to 14.2 Mc. and a signal of 10 mV. fed to the antenna terminal. Note that 10 mV. is (roughly) equal to a "S9 + 40 db." signal. The equivalence may not be exact, but is quoted to indicate that 10 mV. is a large, but not unlikely signal.

The signal generator was then swept over the range 8-25 Mc. (keeping the 10 mV. input constant) and the number of audible beats counted. There is nothing magical about the range chosen—it just happened to be the range with 14 Mc. approximately in the middle.

On all the units tested there were between 10 and 18 spurious responses in the receiver of strengths varying between less than S1 up to S6.

Each one of these spots represented a frequency, which, if occupied by a powerful signal, would give an unwanted "stranger" in the 14 Mc. Amateur band. (Are you absolutely certain that strong teletype signal really is on 20 metres)

In general the possibility of spots can be traced to the use of low frequency heterodyning techniques and the difficulty, at lower frequencies, of removing harmonics from the injection chain.

In this design nearly all the mixing is done at frequencies in excess of 40 Mc., and considerable attention has been paid to the filtering of the injection signal to ensure waveform purity.

Perhaps the real worth of the technique is best demonstrated by mentioning that when the test outlined above was applied to this receiver no spurious responses were detected at all.

## VFO GENERATOR

The circuit diagram is given in Fig. 6 with the associated coil data set out in Table 3.

A 2N3564 bipolar transistor is used in a series tuned Clapp type circuit and covers 9.95-10.80 Mc., i.e. the usual 500 Kc. plus a bit of overlap. The reason for the extra 100 Kc. at the h.f. end will be detailed later. Output from the oscillator is taken from the emitter via a MPF102 source follower to the gate of a second MPF102 mixer. The h.t. to the oscillator and buffer is regulated by an 8.2 volt zener diode.

A third MPF102 acts as an overtone crystal oscillator at 46.0 Mc. The drain coil L14 is tuned by a series combination of 4.7 and 47 pF. capacitors with a low impedance output being taken from the junction of the two capacitors into the source of the MPF102 v.f.o. mixer.

The mixer drain coil L10 is tuned to 56-56.5 Mc. while L11 is a trap set to 46 Mc. to remove any oscillator voltage present. L12 is a second 56 Mc. parallel tuned circuit and uses 22 pF. and 220 pF. capacitors in series to give the low impedance output necessary for the heterodyne mixer section.

The whole generator is contained in a die cast metal box for mechanical and thermal stability. H.t. voltage is fed into the box via a 1,000 pF. feed through capacitor.

## THE HETERODYNE OSCILLATORS

The circuit diagram is given in Fig. 7 with associated coil and crystal data for all bands being set out in Table 4. Only one crystal oscillator is shown, but there is one required for each band. All outputs are paralleled and switching is by application of h.t. to the board required. Once again this technique has been adopted to simplify band switching and to avoid mechanical alterations when adding bands.

One circuit board is used and is "wired" for four bands. Simple mounting of additional components is all that is required to extend to other bands.

The four oscillators on their common board are again contained in a die cast box which is mounted on the chassis directly behind the v.f.o. box. If required another four oscillators can be accommodated in a second die cast box bolted to the lid of the first.

The output frequency of each oscillator may be varied slightly by means of L19 to ensure precise band edge alignment and thus a common dial calibration for all bands.

The drain coil (L20) is tuned by the series combination of the 8.2 pF. capacitor shown in Fig. 7 and the 100 pF. capacitor in the source circuit of the 3N140 injection mixer of Fig. 8.

All outputs are connected in parallel so that, as in the case of the r.f. stages, only one 100 pF. capacitor is needed.

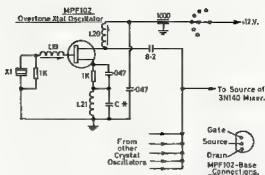


FIG. 7.-4 BAND TRANSISTOR TRANSCEIVER - HETERODYNE OSCILLATOR.

Band	L19 Series Coil	L20 Drain Coil	C <sup>o</sup> pF.	Xtal Freq. Mc.
160	10t., 28g.	11t., 28g.	47	45.20
80	10t., 28g.	11t., 28g.	47	43.50
40	10t., 28g.	11t., 28g.	47	40.00
20	9t., 28g.	11t., 28g.	100	51.00
15	10t., 28g.	11t., 28g.	100	44.00
10	15t., 28g.	20t., 28g.	100	36.00

TABLE 4.-HETERODYNE OSC. COIL DATA

Notes on Table 4 and Figure 7:—

- L21, the source coil, is the same for all bands and consists of 20 turns of 28 B. & S. source wound on a 330K  $\frac{1}{2}$  watt Ducon resistor (9.125" diam. x 0.375" long).
- Coils L19 and L20 are close wound on Necoid Type 722/1 bakelite coil formers.
- All coils are wound with specified gauge of B. & S.

## INJECTION MIXER

A 2N3564 bipolar transistor amplifies the v.f.o. generator output to the level required for the 3N140 dual gate FET mixer. L16, together with the capacitive divider formed by the 22 and 220 pF. capacitors, resonates at 56.25 Mc. The collector coil L22 is parallel tuned by a 22 pF. capacitor and is top coupled by a 2.2 pF. capacitor to L17, also resonant on 56.25 Mc. L18 is a series tuned trap to remove any last vestige

of 46.0 Mc. component that might escape from the v.f.o. box.

Excitation from the crystal heterodyne oscillators is applied to the source of the 3N140 mixer. Gate 2 of the mixer is biased by the 10.0 and 3.9K resistors across the supply rails.

The drain circuit of the 3N140 has an untuned 2.5 mH. RFC as its load and an MPF102 source follower is used to provide a low output impedance.

The whole mixer chain is contained in a small diecast box which is bolted to the top of the v.f.o. generator box.

(Continued on Page 14)

Coil	Freq. Mc.	Turns	Wire Gauge B. & S.
L16	56-56.5	12 (tap 3)	20
L17	56-56.5	12	20
L18	46 (trap)	16	20
L23	56-56.5	12	20

TABLE 5.—INJECTION MIXER COIL DATA

Notes on Table 5 and Figure 8:—

- All coils close wound on Necoid Type 722/1 bakelite formers.
- The RFC in the 12 volt supply line to the VFO amplifier consists of 30 turns of 28 B. & S. wire on a 1 watt 100K resistor.

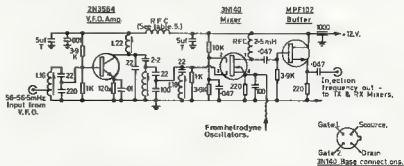


FIG. 8.-4 BAND TRANSISTOR TRANSCEIVER - INJECTION MIXER.

# ROSS HULL MEMORIAL VHF/UHF CONTEST, 1968-9

The Federal Contest Committee of the Wireless Institute of Australia invites all Australian and Overseas Amateurs and Short Wave Listeners to participate in this annual Contest which is held to perpetuate the memory of Ross Hull whose interest in v.h.f./u.h.f. did much to advance the art.

A Perpetual Trophy is awarded annually for competition between members of the W.I.A. in Australia and its Territories, inscribed with the name and life work of the man whom it honours. The name of the winning member of the W.I.A. each year is also inscribed on the Trophy. In addition, this member will receive a suitably inscribed certificate.

## OBJECTS

Australian Amateurs will endeavour to contact as many other Amateurs in Australia and Overseas under the following conditions.

## DATE OF CONTEST

From 0001 hours E.A.S.T., 7th December, 1968, to 2359 hours E.A.S.T., 12th January, 1969.

## DURATION

Any seven calendar days within the dates mentioned above, not necessarily consecutive. These periods are to be at the operator's convenience. A calendar day is from 0001 hours E.A.T. to 2359 hours E.A.T.

## RULES

1. There are two divisions, one of 48 hours duration, and one for seven days. In the seven-day division, there are three sections:

- (a) Transmitting, Open.
- (b) Transmitting, Phone.
- (c) Receiving, Open.

2. All Australian and Overseas Amateurs may enter for the Contest whether their stations are fixed, portable or mobile.

3. All Amateur v.h.f./u.h.f. bands may be used, but no cross-band operating is permitted. Operators are cautioned against operating transmitting equipment on more than one frequency at a time, particularly when passing cyphers. Cross-band operation to assist contest working is prohibited.

Such operation will be grounds for disqualification. Cross mode contacts will be permitted.

4. Amateurs may enter for any of the transmitting sections. The seven-day winner is not eligible for the 48-hour award.

5. Only one contact per band per station is allowed each calendar day.

6. Only one licensed Amateur is permitted to operate any one station under the owner's call sign. Should two or more operate any particular station, each will be considered a contestant and must submit a separate log under his own call sign.

7. Entrants must operate within the terms of their licences.

8. **Cyphers:** Before points may be claimed for a contact, serial numbers must be exchanged. The serial numbers of five or six figures will be made up of the RS (telephony) or RST (c.w.) report plus three figures, commencing in the range 001 to 999, for the first contact, and will then increase in value by one for each successive contact. When a contestant reaches 999 he will then commence again with 001.

9. **Entries must be set out as shown in the example, using only one side of the paper.** Entries must be post-marked not later than 10th February, 1969, and clearly marked "Ross Hull Contest" and addressed to Federal Contest Manager, Box N1002, G.P.O., Perth, W.A., 6001.

10. **Scoring for all sections will be based on the attached table.** Distances must be shown in the log entry as shown in the example. Failure to make this entry will invalidate the particular claim. Some typical distances are given in the attached table.

11. **Logs:** All logs shall be set out as in the example and in addition will carry a summary sheet showing the following information:

Name ..... Call Sign  
Address ..... Division .....  
..... Claimed Score

## SCORING TABLE

Distance in Miles	82 Mc	144 Mc	432 Mc	578 Mc	Higher
Up to 25 Miles	1	1	2	2	20
26 to 50 "	1	1	10	10	80
51 to 100 "	2	5	25	30	100
101 to 200 "	5	10	50	60	200
201 to 300 "	15	15	75	85	250
301 to 500 "	10	20	100	125	300
501 to 1050 "	5	25	200	200	350
1051 to 1500 "	10	50	250	250	400
1501 to 2500 "	20	100	300	300	450
2501 to 3500 "	35	200	400	400	500
3501 to 5000 "	50	300	450	450	550
5001 and over	100	400	500	500	600

Operating Dates ..... (7 cal. days)  
Highest Score over a 48-hour period was ..... points.

Operating period is ..... from hrs. E.A.T. .... / .. / 68  
to hrs. E.A.T. .... / .. / 68

**Declaration:** I hereby certify that I have operated in accordance with the conditions of my licence and abided by the Rules of the Contest.

Signed .....  
Date .....

12. Entrants not abiding by the Rules of this Contest will be disqualified.

13. The ruling of the Federal Contest Committee of the W.I.A. will be final. No dispute will be entered into.

14. **Awards:** Certificates will be awarded to the winners of each section in each VK and Overseas Call Area. The VK contestant who returns the highest score in the transmitting section and who is a financial member of the W.I.A., will have his name inscribed on the Trophy which will be held by his Division for the prescribed period. A Certificate will be awarded to the contestant who shall not be the Trophy winner, and who returns the highest scoring log covering a period of any 48 consecutive hours.

Also, Certificates will be awarded for operating in the Ross Hull Contest and breaking any Australian v.h.f./u.h.f. distance record.

## RECEIVING SECTIONS

1. Short Wave Listeners in Australia and Overseas may enter for the Contest, but no transmitting station may enter.

2. Contest times and logging of stations on each band are as for the transmitting sections, however there is no 48 hour sub-section.

3. To count for points, logs will take the same form as for transmitting sections, but will omit the serial number received. Logs must show the call sign of the station heard (not the station worked), the serial number sent by it, and the call sign of the station being worked.

Scoring will be on the same basis as for transmitting stations, i.e. on the distance between the Listener's station and the station heard. See the examples given. It is not sufficient to log a station calling CQ.

4. A station heard may be logged only once per calendar day on each band for scoring purposes.

5. **Awards:** Certificates will be awarded to the highest scorer in VK and Overseas countries.

## EXAMPLE OF TRANSMITTING LOG (Brisbane Station)

Date/Time E.A.S.T.	Band Mc	Emission	Call Sign	RST/No. Sent	RST/No. Rcvd.	Dist. Miles	Points Claimed
24th Dec. 0100 E.A.S.T.	52	A3(a)	VK7ZAI	68001	59004	1110	10
0110 E.A.S.T.	52	A3(a)	VK7ANG	68002	57051	330	10
0230 E.A.S.T.	144	A3	VK5ZK	58003	65043	960	25
0235 E.A.S.T.	144	A3	VK3ZJO	45004	46021	850	25

## EXAMPLE OF RECEIVING LOG (Perth S.W.I.)

Date/Time E.A.S.T.	Band Mc	Call Heard	RST/No. Sent	Station Called	Dist. Miles	Points Claimed
2nd Jan. 0900 E.A.S.T.	52	VK5ZDK	69221	VK8KK	1330	10
1025 E.A.S.T.	52	VK5ZCF	58195	VK5ZAA	2040	20
1110 E.A.S.T.	432	VK5ZDS/8	67961	VK8LJ/8	60	25
3rd Jan. 0900 E.A.S.T.	144	VK5ZLJ	44102	VK5ZCN	1330	30

# S.S.B. Transmitter—An Amateur Engineering Project

## PART THREE

H. F. RUCKERT,\* VK2AOU

### SECOND MIXER AND CRYSTAL OSCILLATOR

The second mixer is basically identical to the first one. One can use a balanced mixer with a twin triode, and different valves and a variety of operating conditions were tried, or a mixer valve like the 6AJ8, etc., with screen grid shielding to prevent the oscillator signal appearing at the plate may be tried as the writer did.

The following problem occurred: The linear p.a. was on a separate chassis and no tuned grid circuit was provided. The driver tank employed caused, on 10 metres, a substantial downward drive voltage transformation, due to the ratio of driver plate capacity to p.a. grid capacity. Changing the L-C ratio at the driver plate circuit did not help much due to mismatch.

The 12BY7 driver used at the time was already working in class AB1 and could not take a higher grid input voltage (or grid current would occur, causing flat-topping) to obtain more drive on 10 metres. The gain, using a 6BA6 pre-amplifier with wide band damped tuned circuits, was only about 4, and the second mixer 6AJ8 gain was 1.5 to 2 with a similar tuned circuit. This mixer could not be driven harder without causing distortion here or in the first mixer. A further difficulty was encountered due to the crystal oscillator being remote in the nearby standing receiver, operating at the 1-2 volt level required for the receiver 6U8 mixer valve. Less than 1 v. r.f. was left at the end of 18 inches of co-axial cable at the transmitter second mixer.

The mixer input signal should be no higher than 10% of the oscillator voltage, which means that under these conditions the placement of stages made it impossible to obtain sufficient drive for 15 metres and the two 10 metre ranges. At this stage one can either scrap the design, pull everything to pieces and start with a new chassis again—if one feels like it—or solutions have to be found which can easily be incorporated. There was no space for additional valves and tuned circuits with band switches.

It was found that a ferrite balun transformer with 4 x 8 turns (the type used as t.v.  $\frac{1}{2}$ " x  $\frac{1}{2}$ " aerial balun) gave a voltage gain of 4 over the required range from 8 to 33 Mc. and matched the 300 ohm co-axial cable between receiver and transmitter mixer. This balun was a most efficient wide band amplifier.

The second mixer was slightly modified to suit the available 8-10 v. oscillator voltage, making it possible to use 1 v. s.s.b. input signal. The output of 2 v. s.s.b. signal was twice that delivered by the 6AJ8 mixer. It would have been a great help if the published equipment descriptions had shown the d.c. and r.f. voltages and d.c. currents.

The crystal oscillator circuit is usually used with overtone crystals like those

here employed for the 15 and 10 metre operation (25.45, 32.45 and 32.95 Mc.), but works just as well on the fundamental frequency of the other crystals. Band switching is so very much easier than with the circuit recommended by the crystal manufacturer. A 6AM6 triode connected in pentode connected buffer stage is used, which gave more output than a cathode follower which was also tried. This was a matching problem. The grids of cathode followers must not be driven into grid current, as sometimes insufficient voltage is obtained also due to unity gain of these stages. Next time the c.o. will be placed close to the second mixer.

Trying to use surplus crystals which were etched or lapped to the frequencies required was only a disappointing experience. With these the receiver had many more spurious beat notes than those precalculated, and the output was too low on overtones or harmonics. The new locally manufactured crystals were perfect in every respect. They were the only expensive item the writer had to buy to build this transmitter. The 10 pF. and 7 pF. series capacitors pull these crystals to the required frequency.

### PRE-AMPLIFIER AND DRIVER

To be able to step up the drive power the 6BA6 pre-amplifier was replaced by a 12BY7, and the 12BY7 driver was replaced by a 6BQ5 pentode. These valves with their higher plate current operating in class AB1 match better the damped wideband tuned circuits. Plenty of clean drive is now available on all bands.

Using valves with relatively high grid 1 to plate capacity may call for neutralising. In this case, good shielding between stages, a small earthed plate between grid and plate valves, stray field preventing Q2 ferrite slugs in the coils (not in driver plate coils), grid stopper resistors, ferrite stopper rings at grid 1 and plate of the driver, the driver loading by the final space charge capacity effect, and the anyhow necessary damping resistors parallel to tuned circuits kept things under control without neutralisation.

With the different L-C ratio of the tuned circuit and damping resistors, these two stages are able to deliver uniform drive power at 55 v. r.m.s. to the final at all operating frequencies between 3.5 and 29.0 Mc. Minor deficiencies can be compensated with the drive control (5K ohm) in the cathode of the 12BY7 (ratio 1:3 at the most). The pre-amplifier tuned circuits are tuned to frequency 10% higher than the lower band edge, and the second mixer plate tuned circuits are set to a frequency 10% below the upper band edge. Under these conditions the 12BY7 has a gain of up to six and the 6BQ5 achieves a gain of six at 10 metres and 20 at 80 metres after pi filter transformation (measured at the grid

of the final) with the driver plate circuit tuned to the exact working frequency.

### LINEAR POWER AMPLIFIER

This transmitter occupies a quarter of the volume the a.m. rig it replaces, and the weight is also down to 30%. On the other hand, there were no plans to build a minibox without leaving air space inside to fit in the glove box of the car. It should be possible to run the final at full legal power all day and not just for 30 seconds as recommended by some transceiver manufacturers (tune-up condition) to prevent the glass of the final valves from softening. Using a 200w. capability exciter followed by a 400w. linear does not appear very economical either. The final valves were to be operated close to the manufacturer's class AB1 specifications.

There were still the 25 years old but very modern looking all glass Telefunken radar valves, Type LS50, in my collection. Their size is similar to the 6146 but plate dissipation is 40w., which is ideal for the experiments intended to be carried out. Their plate current was only half that of the 6146, but by using three valves in parallel with slightly higher screen and plate voltage the legal power max. of 400w. p.p.s. output with double tone input and zero grid current could be obtained with 55v. r.m.s. as drive potential.

The total valve capacities were similar to 1 or 2 more modern valves:

For three valves in parallel—  
Input C: 45 pF.  
Output C: 30 pF.  
Grid-Plate C: <0.27 pF.  
gm: 12 mA/V.

The valves require little filament power, being 12.6 v. x 3 x 0.75a.

There is not much wrong with certain older valves, and I am grateful to DLIFK for a few more valves of the same type.

Also the three valve holders of the linear p.a. are mounted above the chassis. Their connecting pins (except grid 1 and plate) are soldered to tubular 1,000 pF. feed-through capacitors, 0.01  $\mu$ F. disc (marked) capacitor are soldered parallel to the 1,000 pF. capacitors—just in case. A shielding strip runs across the valve holder and through a slot between grid 1 and plate pin.  $\frac{1}{2}$ " wide sheet copper strips have been used to wire r.f. carrying components.

At first no v.h.f. plate suppressors were used when the transmitter worked only on 80, 40 and 20 metres. Some instability was observed on 15 metres, and something had to be done before 10 metres could be used. The usual 50 and 100 ohm resistors with a few turns of wire wound around the resistor as a choke were working fine on 20 and 15 metres, but on 10 metres these resistors went up in smoke. It was found that more than two turns caused such



a r.f. voltage at the 50 ohm 1 watt resistors that they were overloaded.

Finally two turns of  $\frac{1}{8}$ " wide silver plated copper bands were wound around the 1 watt 50 ohm carbon resistors. This method had the desired effect without reducing the output on 28-29 Mc. Q1 ferrite rings were used before; they were effective as suppressors, but caused a loss of power above 21 Mc.

R.f. power measurements with a 52 ohm dummy load (resistor in oil filled container) and r.f. amp. meter showed that the output at 21 Mc. and especially at 28 to 29 Mc. fell off too much compared with the performance at 3.6, 7.1 and 14.2 Mc. A few calculations (A.R.R.L. Handbook) made it clear that the total pi filter input capacity at 28 Mc. should be 40 pF. for the plate load of 1,500 to 2,000 ohms and a loaded circuit Q of 12.

The output capacity of the three valves, the substantial stray capacity from the band-shaped leads and other connected components, and the tuning capacity of the variable air capacitor had each about 30 to 35 pF. This means that on 10 metres the C was two to three times too large and the resulting L was just as much too small. The L/C ratio was four to nine times too low.

With nearly half the L distributed as leads between components and switches the tuned circuit had radiating losses, and it presented a mismatch for the valve (generator). Series tuned tanks are used at 2 metres and a similar technique is employed in recent transmitters where up to 10 t.v. line output valves are operated in parallel (mobile kw. tx, etc.). Between the hot end of the pi input capacitor and the high voltage end of the pi coil is, at 21 Mc., a 95 pF. and at 28 Mc. a 35 pF. capacitor series connected to bring the total effective C (parallel to the pi coil) to about 62 pF. at 21 Mc. and to about 40 pF. at 28 Mc. The correct L can now be used and the L/C ratio and circuit Q now reach the right values.

10 pF. and half a 10 metre coil turn more or less make quite a difference to the matching and r.f. output, the drive requirements and grid current starting point. As long as coils get hot (taps may even unsolder) and the valve plates turn red, one can be sure that

a mismatch caused it. The extra series tank capacitor and the input variable capacitor may both be a ganged variable unit. The series capacitor needs in this case a 30 to 40 pF. fixed capacitor in parallel. These capacitors must be able to take the very substantial circulating current at 28 Mc. and about half the r.f. plate voltage. I used fixed ceramic 1.5" diameter 10 kVA. NPO transmitter capacitors.

In order to increase the lumped L of the 10 and 15 metre coil, the lead inductance of the whole circuit had to be reduced. This is not easy with large components, the many switches and a certain front panel layout. It was achieved by using  $\frac{1}{8}$ " to  $\frac{1}{4}$ " copper band instead of round wires. Furthermore, the two 4" to 5" long leads from the switches to the two air capacitors (106 pF. and 450 pF.) were made of two parallel running copper bands which were only connected at the ends.

All these measures allowed to use 5 turns instead of only 3 turns for the 18 metre coil, which doubled the L value, solved the matching problem, 28-29 Mc. tuning, L/C ratio and Q. The r.f. output was markedly increased at 21 Mc. and especially at 28-29 Mc., reducing at the same time the dissipated plate power. The tuning range becomes too narrow and the power output drops again if the series capacitor is made too small.

At an earlier stage, two H1 ferrite rings were placed over the common grid lead of the p.a. valves. This step was later found to be unnecessary and quite wrong, because they prevented 80% of the 10 metre drive voltage from reaching the final stage, like a good low pass filter.

The usual neutralising via a partly by-passed lower end of the p.a. grid (or driver plate) tuned circuit could not be used in this case. R.f. with opposing phase is also available at the output end of the pi coil of the final tank. So a series connected 3 pF. and 3-30 pF. trimmer capacitor provides an effective neutralising loop, which was only necessary on 20, 15 and 10 metres.

To adjust the neutralisation, the transmitter was warmed up and tuned up on an aerial with less than 1:1.5 s.w.r. Next, plate and screen voltage was turned off. The remaining r.f.

voltage at the plate tuned circuit is measured with a r.f. probe v.t.v.m. with drive applied as before. The trimmer is adjusted until a minimum below 1v. is found. Detuning of the tank to an off resonance position or the use of an aerial with 1:3 s.w.r. will upset the balance, but with reasonable correct tuning, tank loading and low A.W.R., complete stability is assured.

Difficulties were earlier experienced when the transmitter was tuned up with an improvised dummy load consisting of two 200w. light globes. Even these two globes had in parallel 150 ohm impedance when running cool. Adjusting the transmitter and neutralisation with the unstable dummy loads (impedance depends on heat caused by the power applied) proved misleading and wrong. Depending on the accuracy of the driver tank tuning, regeneration occurred at modulation peaks after an aerial with low s.w.r. had been connected. This condition was also reported as audio distortion. No difficulties are observed with a 52 ohm Heath Antenna dummy load. This matching sensitivity of this form of neutralisation was also the reason why the multiband tank universal aerial coupler originally installed was later abandoned.

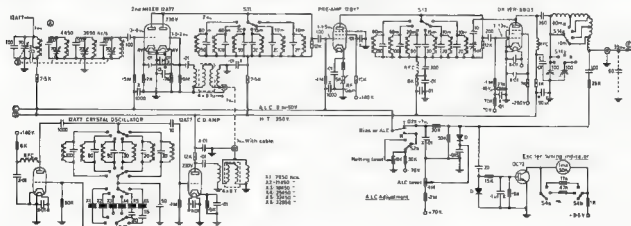
The final pi tank uses  $\frac{1}{4}$ " diameter ceramic transmitter capacitors of 75 pF. and 270 pF. at the high r.f. voltage input end, and medium heavy mica transmitter capacitors at the output end to extend the values of the variable air capacitors.

#### S.W.R. METER

The s.w.r. meter is actually a double r.f. watt meter which reads practically frequency independent, and it can be adjusted for different load impedances, features few popular s.w.r. indicators have. It is important to note that the shielding braid of the co-axial cable going through the Q2 ferrite ring is only earthed at one end.

Adjustment: The output is connected to a true 52 or 75 ohm resistor capable of handling about 20 watts or more. With some power applied, one has to see which trimmer allows to adjust zero meter reading. The co-axial s.w.r. meter connections are now reversed.

DLQ1, "DL-QTC," February 1968.





and the other trimmer is set to obtain zero reading. The resistance of the meter movement including shunts and dropping resistors represent the diode load and determine the diode characteristic and s.w.r. reading obtained. This meter was an r.f. amp. meter with burnt out thermo-cross. The meter scale figures are, at low s.w.r. levels, nearly the right s.w.r. values, as a calibration with various load resistors showed

Forward reading four divisions, 52 ohms, 1:1 s.w.r.

Reverse Reading (Original Marking)	S.W.R.
1.8	1.5
2.25	2
2.5	2.5
2.75	3
2.9	3.5
3.15	4
3.3	5

The two Ge diodes should be matched. This w.c. and r.f. watt meter serves also as p.a. tuning indicator.

## POWER SUPPLIES

Heavy filter chokes, large paper capacitors and the 866 rectifiers are now obsolete. The silicon diodes and high capacity electrolytic capacitors take their place.

Exciter and final p.a. have their own power supplies built in, providing also regulated negative bias and regulated lower B+ voltages. The mains switches S15 (a, b, c) and S16 (a, b, c) have four positions:

- (1) Off.
- (2) Filaments and negative bias on.
- (3) H.t. and lower B+ on, via 1K ohm resistor to limit voltage and current peaks and to slow down the charging of the electrolytics.
- (4) Shortening the 1K ohm resistor to reduce circuit resistance to improve h.t. regulation.

To be able to use the available 2 x 350v. transformer for the exciter supply without obtaining a too high B+ voltage, not to make dropping resistors necessary which cause extra heat, small charging electrolytics were only used. These 2 x 4  $\mu$ F. capacitors must be able to stand up to the so-called high ripple voltage and current without exploding.

The 220v./2 x 800v. h.t. transformer has been re-impregnated after its first

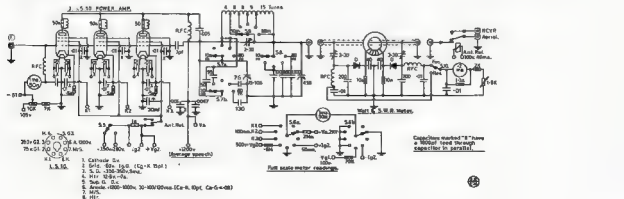
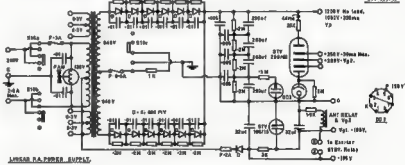
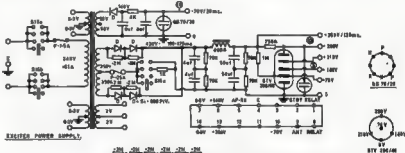
20 years of service which stopped some strange noises. With 240v. input, 2 x 940v. output are obtained. No filter choke, only a string of four 260  $\mu$ F. (200  $\mu$ F. nominal) electrolytic capacitors are used here. It may be vital to remember that the aluminium can is usually not insulated from the electrodes of the unit, no matter whether the positive and negative terminals are both available at the insulated base plate. Insulating sleeves are placed between can and clamp. Shunk-on plastic sleeves some capacitors have may not be sufficiently safe, they can crack if the components become too hot. A red neon pilot light indicated the charge of the electrolytic capacitors.

The bleeding action of the resistor chains, VR tubes and the screen current drain is quite rapid. Two screen grid voltages are available with the switch S5 from two multi-section neon stabilisers. A 30  $\mu$ F. electrolytic capacitor provides the extra screen grid power for occasional load voice and drive

peaks, without having to use larger stabilisers capable of holding the voltage at >10 mA. screen grid current per p.a. valve. The h.t. voltage fluctuates with speech (a.s.b. modulation) by not more than  $\pm 3\%$ . The transmitter power is limited by the allowable heating up of the h.t. transformer, the screen grid current the 1SS0 valves can take, and the regulation limitations of the U<sub>2</sub> stabilisers.

A convenient source for the -80 volt bias and 100 volt/40 mA. for the antenna relay was found at the centre tap of the primary winding of the h.t. transformer. A separate 200 mA. fuse was used. At one stage an electrolytic capacitor had lost its capacity, and did not therefore act as a charging capacitor any more, and so the stabiliser for the bias voltage did not fire, causing high bias voltage of the wrong value and ripple. Strong carrier and distorted audio was reported. The large capacitors now used leave only a few mV. ripple voltage.

(To be continued)



# Solid State Transceiver

(Continued from Page 9)

# Overseas Magazine Review

Band	Signal Mc.	Injection Mc.	S.B. Generated	Hetro. Xtal Mc.
180	1.8-2.3	10.8-11.3	LSB	45.20
80	3.5-4.0	12.5-13.0	LSB	43.50
40	7.0-7.5	16.0-16.5	LSB	40.00
20	14.0-14.5	5.0-5.5	USB	51.00
15	21.0-21.5	12.0-12.5	USB	44.00
10A	28.0-28.5	18.0-19.5	USB	37.00
10B	28.5-29.0	19.5-20.0	USB	36.50
10C	29.0-29.5	20.0-20.5	USB	36.00
10D	29.5-30.0	20.5-21.0	USB	35.50

TABLE 6.—FREQUENCY DATA

Notes on Table 6:—

- In all cases the 9 Mc. sideband is generated on USB. On 180/80/40 this 9 Mc. USB is subtracted from the injection frequency to give LSB. On all other frequencies it is added to the injection frequency to give USB.

## AVAILABILITY

As indicated in the previous article, kits and/or board and/or instructions will be made available at the following prices:

- (1) VFO generator complete with crystal and die cast box, \$35.25 each.
- (2) Injection mixer complete with die cast box, \$19.75 each.
- (3) Hetrodyne oscillators—  
(a) 1st board, including board, die cast box and crystal, \$16.50 each.  
(b) 2nd, 3rd and 4th boards, components and crystals, \$9.50 each.
- (4) Receiver front-ends—  
(a) 1st and 3rd bands, including boards, \$9.75 each.  
(b) 2nd and 4th bands, components only, \$7.75 each.

Postage on items 1, 2, 2a is 20c; on items 3b, 4a and 4b is 15c. Please address enquiries to 4 Eliza-beth Street, East Brighton, Vic., 3187.

## ERRATUM

Would readers please note an error in the circuit diagram of the receiver audio section (Fig. 2, Nov. 1968 "A.R."). A connection is shown between the collector of the AY1121 driver transistor and the 12-20 volt h.t. line. This connection should not exist and the AY1121 collector is connected only to the base of the AY1120 device.



## FORMER EDDYSTONE CHIEF HERE

Mr. Arthur Edwards (G6XJ), formerly managing director of Eddystone Radio (Stratton & Co. Ltd., Birmingham, U.K.), arrived in Melbourne on 4th December. An active Amateur, Mr Edwards will stay in Australia for an indefinite period and will be operating call sign VK3AMM portable.

## "RADIO X3"

**June 1968—**  
**A De Luxe Mobile Power Supply:** L. Dye and D. Brook. Using 2N2095s (18v) to produce 850 volts at 160 ma. from 14v. battery. Efficiency about 80 per cent.

**Be It With Diodes:** C. de Souza. Discussion on using diodes to protect a number of electronic circuits.

**July 1968—**

**The Ferrite Balun;** J. Hugo. ZS1SC Describes a method of making a balun using straight ferrite rod ½ inch diameter. Loopstick places about three inches long should be suitable 1/1 and 4/1 baluns can be made with this method.

**Know Your Quad:** H. Randall. ZS1HF General discussion on the origin of the Quad antenna and information on its characteristics.

**Max Erection Without Tears:** T. Curt. ZS1-22. Describes a method of easily erecting a guyed mast using a gin pole.

**August 1968—**

No technical articles.

## "OZ MAGAZINE"

**August 1968—**  
**Converter for 150 Mc.:** Flemming Rasmussen. Describes a transistor converter using tough lines.

**Receiver with Ceramic Filter:** H. Stillerup Rasmussen. Describes a solid state receiver for the Amateur bands using ceramic filters in the I.F. stages.

## "SHORT WAVE MAGAZINE"

**June 1968—**  
**8K Band C.W. Transmitter:** Described as "a modernised version of a standard design" incorporating rx pre-amplifier, break-in and fully key controlled. Runs about 100w. to 4165 V.h.f. Working by Mieser. Terminology, procedure, method, equipment and example.

**Some Gelson VFO/Killer Modifications:** Some suggestions for improving the stability, h.f. band drive and note of transmitters using these popular units.

**Vertical Aerial Systems for the Communication Bands:** Materials, methods of mounting and a co-axial dipole for ten metres.

**July 1968—**

**Practical Two Metre SSB Transceiver, Part I:** Design, circuitry, construction and alignment. 80w. on a QV90/40.

**Teasing Silicon Diodes:** Tells how to determine peak inverse voltage, etc.

**Basic VFO for Multiband Operation:** At first sight it looks a little like a Gelson. Tubes used are 6C4 and 5763. Clapp oscillator circuit is used.

**Station Central System:** Ideas for circuit arrangement, describing a practical case.

**Notes on Joystick Operation:** Loading up, use of a.t.u. and s.w.r. indicator. This should interest some of those who have bought Joy-sticks.

**Small Transistor Tx for Two Metres:** Describes a small unit with an output of about 100 mW.

**September 1968—**

**Controlled TX/PSU for Standby Operation:** G6PG Describes a small, 15w two stage single band tx and 300v 80 ma. power supply; for 1.8, 3.5 or 7 Mc.

**Simplified Transceiver for the Two Metre Band:** G6JQV. Author describes unit he built for 2 mhz from an old low band module and suggests how it can be adapted for 4 mhz. May appeal to 3 and 6 mhz men.

## "RADIO COMMUNICATION"

**June 1968—**

**8 Mc SSB Phasing Kandler Using VFOs:** G6NJD discusses the theoretical approach to the problem and then gives a practical solution. This article could be of major interest to v.h.f. s.b. addicts.

**Reflexometers and Directional Power Meters:** G6NJD goes into the theory of operation of these devices complete with the mathematics. He then describes a device which differs from the usual v.w.r. meter because it is not sensitive to changes in the operating frequency. Describes a four core cabinet, G6JQV describes a simple method of making acceptable cabinets from readily available components with the

tools which will normally be available to the average Radio Amateur.

**The British Trans-Arctic Expedition:** G6FLB describes the preparations for the expedition encountered by the party which is at present attempting to walk across the ice from Point Barrow in North America to Spitsbergen. Previous attempts have failed to record that the ice is in constant motion and have walked against the current as it were. The present expedition is using the current to help them on their 3,800 mile journey on "Shank's Pony".

**Technical Topics:** In this issue Pat Hawker, G4A, discusses on transistor repair jobs, thyristor control circuits and the interference they can cause unless the equipment incorporating the thyristor is properly "suppressed" and shielded. A new type of transistor mixer, patented by CFTH-HB is described. This is covered by British Patent No. 1,104,888. Common collector configuration is used and although the circuit has practically unity gain, this device is for very low noise and is not nearly so lossy as diodes. The circuit is said to overcome the transistor saturation problem. "Another Crystal Oscillator" circuit operating in the parallel resonance mode, with fundamentals between 1 and 20 Mc is used.

Pat Hawker also discusses the articles which have recently appeared regarding some of the developments in "Computer Aids" such as "The Army Loop" described in "QST", March 1968.

**July 1968—**

**A Simple Solid State Sideband Sender:** W. B. Hartog, G2JEZ. They've gone all German in the title. A brief look indicates that this article contains some useful ideas for the man who wishes to "roll his own" in the face of all the opposition from the manufacturers. A Selection of Co-axial Connectors, Mrs. K. M. Priestley, G6JQV. The authors describes most of the inexpensive type co-axial connectors available on world markets and tells of the advantages and disadvantages of some of them.

**Technical Topics:** This month Pat Hawker talks of the advantages of Morse, simple product modulator, new monolithic filters, the latest development in the crystal filter field. "A Modern ECO", a new v.f.o. antenna and various types of recent v.f.o. circuits such as the Seltzer and Vackar using FETs.

**The Idea Behind G6BLO:** G6BLO is the star of the S.C.S.B. set up at the 1968 "City of London Festival". Sylvia Mearns discusses the concept and what is expected from the "advertising" that British Amateur Radio is receiving.

**A Fresh Approach to the TVI Problem:** Various ways of preventing spurious signals from being generated by a transmitter are discussed for preventing "spurious Amateur Radio" from being generated in various pieces of entertainment equipment.

**September 1968—**

**Long Aerials:** G6NA. A discussion of loop aerial characteristics and their uses for transmitting and receiving.

**A Simple Audio Oscillator and Pulse Generator:** ZL5AMJ. Using parts of the type we can get in Australia, the author describes a sine wave oscillator with a frequency range of 15 cps. to 130 kc output 5v. pp. sq. wave covers the same range and has a variable "control" ratio.

**Technical Topics:** G3VA. This month Pat Hawker ranges from "Transverters to Modulators" and "Communication", a.s.f.m. and a.f. filters are by the way.

## "DL-QTC"

**September 1968—**  
**Multiband Quad:** DL4VM. A different sort of quad. The elements each consist of a triangular closed loop on each end of the boom and the whole thing is held by tuned feeders from a matching unit. Both ends are driven. For 20, 15 and 10 metres.

## "QST"

**July 1968—**  
**The M.A.R.A.T. Antenna:** K1KLL. This looks like a reasonably practical version of the "Army Loop" applied to mobile. It is built of rectangular down pipe and looks like an overgrown picknick.

**Waste Less Drives:** W6SKGP. Symbols, nomenclature and principles.

(Continued on next page)

**Integrated Circuit Frequency Divider; KCMZF.** An application to the Amateur frequency standard.

**The Chipboard, W6WYD.** A simple experimental circuit board.

**Some Ground Rules for Sweep Tube Linear Amps; Design; W1CER.** Four 6KD6s as e.p. triodes with individual bias adjustment for each tube to avoid purchasing a "twang" and matching them. 800w. input with 960 volts.

**The Double Baxekas Antenna; W2TV.** Broad-band dipole using co-axial construction.

**August 1968—**  
**The Conscientious Bond Boy; W1CER.** Doug De Maw describes a solid state transmitter for 1.5 Mc Super-regen. tx and tx running about 4w. input.

**A 65 Foot Crank Up; V1EASZ/W6.** Quite a few of these who are really good with things mechanical.

**Digital Counter with Teletype Print Out; W2KBN 1CA.** etc., in a sophisticated piece of equipment.

**The 88B Mark I, V2E1B.** A simple transistor transmitter for 20 and 75 (80) metre sub-band.

**A Transceiver Monitor using Transistors; W1E8X.** For those whose transceivers do not incorporate a monitor, this could be a handy addition. Short and simple.

**September 1968—**  
**A Transmitter Phase Rig for 1.6 Mc; W1CER.** Solid state for the "top band". Input power is 7-8 watts.

**600 to 25,000 Metres, W1E8X.** A simple transistorized converter for the v.l.f.

**The C-Line Matchbox; W1QKQ/ASGKP.** Simplified impedance matching on v.h.f.

**A Tester for Crystals and Transistors; W1NPG.** The title describes it.

**The Two Tailed Monster; W1E8X.** The recipe is to take one four element multiband quad and add tails to the boom to resonate it as a rotatable dipole on 40.

**The 27/MHz. K1E2M.** Running 1.5 watts a.m. with 3 meters, 3 meters.

**Notes on the Vacation Special, W1YTM.** Described as "a tunable filter for the BC4M and an improved 50w transistor modulator for the BC4M". There are still enough of the Commands around to interest VKs.

**Inductance and Q of Modified Baxekas Toroidal Inductors, W1NQN.** Something for the r.l.y. boys.

**General Purpose VFO; W1CER.** Solid state, of course.

**Prefabricated Portable; W6WYT and W6WST.** Described as portable made up from various modules which are readily available on the market.

**Reviews the Strap Box; K1ENU.** Describes some of the traps into which Amateurs can fall if they do not have proper test equipment to test the junk box and disposal items they propose to use.

**"73 MAGAZINE"**  
**July 1968—**  
**Let's Build a Tower; VE1TG.** Sturdy wooden construction for portable use from various parts.

**W1Y: Not a Telling Tower; W5DL.** With this method why not?

**40 Fast Nan Conducting Skyhook; K7V8Q.** Making a part of a drone pole.

**Burn Protection; V2E1B.** A safe place for the hot soldering iron.

**The Beam Pole; W7GJ.** Another phone pole idea.

**Tell That Tower; W1AJW.** Using the house for leverage.

**W1E8X: Great Flyer; Ives.** Another idea to fill the holes.

**IC Audio Amplifier and Oscillator; W1AKS.** W1E8X is in it.

**The New Tower; W1QXT.** Battling the tower inspector.

**Some Audio Thoughts; W1KEM.** Veratilla modular unit.

**BB, W3EAP.**

**More on Crystal Etching; K1GKP.** Using readily available chemical.

**August 1968—**  
**Terminated Grid Linear Amplifier; W1D1S.** Excellent stable configuration. Two 6E6s 4.400As for 2 kw. input. A little too large for Australians.

**Photographic Printed Circuit Process; W6ATZ.** Printed circuit etching made easy. Now who is interested in making their own?

**A Simple Method of DSB Conversion; K1JLL.** An easy way to d.s.b. using a "balun" for broad-band feed. Seems good.

**Basic RF Receiving Converter; W1DZM.** Getting more from your h.f. receiver. Simple circuit using two twin triodes.

**Three on 20 for 15; W1AYVQ.** \$15 three element beam for 30 m. Seems practical, no more beams and no elements with some lightweight wooden members.

**The Mini-Beam Quad; V2EFS.** Efficient quad with spider array. Some handy ideas for an inexpensive easily made quad (three-band variety).

**The Coilless Resurrector; W1D1VD.** End fire array without sacrificing performance. A simple wire array for 30 m. with a gain of 7.7 db.

**A Microphone Preamp; W1E8X/V1.** More speech power without distortion. Simple transistor/diode affair built into a hand mike.

**Review—The Heath IM-37 VTYM; W1QK.** A review of test equipment. The writer reviews the Heath battery operated solid state voltmeter.

**Headlines; KEMVE.** A veteran writer tells how an article on how to write articles for Amateur magazines.

**A Grounded Grid Linear Amplifier; W1WU1.** 3 through 35 Mc. in five steps. Circuit suitable for 4E2Ts or 813s. Cathode driven linear for 800 watts input.

**September 1968—**  
**Going VHF in the Mobile; W1H9F.** Describes how to get the most out of both v.h.f. and UHF.

**Communicator Rebers; W1H9X.** Double conversion of the Gonnet Communicator makes the unit more selective and useful.

**SSB Amplifier; W1AJW.** Although Frank C. Jones is an old timer, he describes solid state equipment using a FET for 432.

**Quick Conversion; W1E8X.** Describes how you can use obsolete v.t. tuners to quickly assemble Amateur band converters.

**Do You Think You're on Frequency; K. Sessions.** Methods of determining frequency on the v.l.f. bands are discussed.

**Parallel T Network Design; Jim Kely.** Seems that there is a lot of work in v.l.f.

**The VESAT Moonbounce Reboiler; W1H9D.** Wayne describes some of the tricks Ray got up to, to make two-way moonbounce contacts with S.E.A.

**6 Wire Ketter; W1E8X.** A handful of transistors and a 6CL6 on 6.

**Six Meter Transceiver; W1AJW.** Using transistor tubes, i.e. b.c. tx and a few extra to produce a small solid state transceiver for 8.

**Two Sideshows from the Two-er; W1AKS.** Quick and easy d.s.b. on 2 m.

**"CQ"**  
**July 1968—**  
**Modulation Unlimited, Part 1; W3PHL.** A two-part article which is completed in the "CQ" August.

**"Super Modulation"; L.e. modulation which exceeds normal a.m. 100 per cent. figures on sensitive peaks, but not on negative peaks.** Covers the principles and circuit techniques necessary to exceed 100 per cent. modulation without the production of undesirable side products, such as distortion and spurious. The modified final power amplifier circuit can be used for c.w., a.m., d.s.b. and s.s.b. modes.

**Veridical Antennas, Part 1; W1E8X.** Describes theory and practice of this type of antenna which the author claims has never previously been covered in depth in an Amateur magazine.

**The Drake SSB VHF Equipment; W1E8X.** Review of the equipment for v.h.f. offered to Amateurs by the Drake Co.

**Veridical Antennas, Part 2; W1E8X/V1.** Describes the various types of Veridical antennas made to Heathkit DX100 putting ideas into operation.

**The Heathkit HW-100 Transceiver; "CQ" Review.** This is Heath's low priced \$240 (US) five-band unit which according to this reviewer gives a very good account of itself.

**After reading this review, it is certain you wouldn't want to spend \$250 (US) for the SB101.**

**Veridical Antennas, Part 3, Paul Lee** concludes his dissertation on this topic.

**RF Feedback in Audio Compressors; K1E8A.** Short article on elimination of r.f. feedback.

**The Shesbee Symposium; W1E8X/V1.** This article has two parts. Part I describes the first in 1966 and Part II in "CQ" July 1967. This article describes methods of overcoming the various problems which have been encountered by builders of a linear which can be set to run inputs of from about 800w. to 2,000w. peak a.c. according to the number of tubes used in parallel.

**The new 6AS6, which has a special rating of 300w. for 30 sec., should be very suitable for this circuit.** After reading this and its competitors equivalent, you'll find it very easy to find its way into many of the newer transceivers which are operated at 500w. input level. There is a mistake on the circuit shown on p.

**SSB Reception With Signal Frequency Inverter; V2E1B.** Seems to me like a new method of doing it the hard way.

**A Name-Brew Broad-Band Transmuting Balun; W1E8X/V1.** The balun described is made from a length of co-ax wound on a plastic core, 1/2 inch 1/2 inch.

**The same technique could be used with 75 ohm cable to give 75 ohm balanced to 75 ohm unbalanced connection.**

**Wideband RF Pre-Amplifier; W6WYT.** Describes a low noise broad-band FET/transistor amp. with a gain of 25 db. up to 15 Mc. with a noise figure of 1.5 db. Some people may be interested in this technique. My personal reaction is that one would lessen interference by using a tuned device.

**Upgrading the SB-100; W6WYT.** Modifying the Heath SB-100 to improve its a.v.c. system.

## A TRANSVERTER

(Continued from Page 8)

say another 12BY7, and then have the 6CN6s in passive grid, or semi-passive grid.

No attempt has been made to use this transverter on 21 and 28 Mc. by bandswitching, but this should be fairly easy. The same crystal oscillator and buffer amplifier circuitry would be used, and the same crystal. You would have to switch the tuned circuits in the converter, the coil in the plate of the mixer, and the final tank coil.

All tuned circuits in the converter, the oscillator and the buffer are slug tuned. No coil data are given, except that all coils other than the final grid and final plate are on 7 mm. formers. Injection to the 807 is by 3 or 4 turns over the end of the 6AM6 plate coil.

I will be glad to answer any mail queries, provided that they are accompanied by a self addressed stamped envelope, and provided that you don't expect overnight service.

## Publications Committee Report

At the November meeting correspondence was received from BM2DG, VKs 3AQ, SOC, 3AMK, 5HI, 5RG, 7KJ, Nola Sturke, E. Foxon, W. Morgan, and LT981. Technical articles arrived from VKs 2JR, 2SA and 3ZNV. Due to the lack of figures, the financial position of "A.R." could not be ascertained accurately, but it was estimated that the position is reasonably satisfactory.

Efforts to increase advertising content are proving fruitful, the advertising representative says. He has already signed up number of new advertisers and recovered some of those lost several years back. A major effort will be made in this direction during November.

A review of technical material on hand revealed sufficient available to see us through to the February issue, and extra material, particularly short articles, are badly needed.

Progressive results of the November questionnaire were discussed and a very good initial response was noted. No replies had been received from VKZ, but this was thought to be due to the postal strike in N.S.W. having delayed the delivery of the November issue. Over 200 replies were received within 48 hours of "A.R." being mailed. Initial sorting has commenced, but until many more replies are received, no attempt will be made to compile the list.

At the suggestion of the VKS Divisional Council, the committee gave consideration to making token payments for technical articles published. After lengthy discussion, it was agreed that although the suggestion held considerable merit, and in fact conformed to the wishes of the committee as outlined nearly three years ago, it would be better held over for a minimum of a year in order to obtain additional income (if any) we can acquire. In the meantime, we will continue to make the annual awards for selected articles, as we have done in previous years.

The value of the monthly Publications Committee Report was questioned, and the general opinion was that the time compiling it could be better spent as it has to be done during our busiest time of the month. It was, therefore, decided that despite the fact that it has produced some of the best of Federal Convention policy motion some years ago, the report would be discontinued as from this issue. Technical articles and correspondence will be acknowledged by mail in due course, and the Executive Committee's correspondence published in the magazine, for which no acknowledgment will be sent.

All Call Book orders have been fulfilled. Any Division or club requiring additional copies should contact us, as we have a small surplus available.

## SILENT KEYS

It is with deep regret that we record the passing of the following Amateurs:

VK1PI—Les Pitts  
VK2AYA—G. A. Ahlstrom  
VK2AYB—Sid Burton  
VK3VO—Raymond Clark

## TESLA EQUIPMENT IN AUST.

The internationally famous Tesla electronic equipment is now available in Australia through Charmac Industries Pty. Ltd., Eitham, Vic.

Founded in Czechoslovakia 60 years ago, the Tesla company now employs 75,000 people in 50 factories and manufactures heavy electrical and telecommunications equipment.

Charmac Australian sales manager, Les Baker, advised "A.R." that in addition to the range of Tesla tape recorders and audio amplifiers, they would distribute Tesla components, and Agfa tape which had been found most suitable for use with Tesla recorders.

An associate company, Audio-Lec of Australia Pty. Ltd., will distribute the Italian made "Incis" audio equipment.

## W.I.A. D.X.C.C.

Listed below are the highest twelve members in each section. Position in the list is determined by the first number shown. The first number represents the participant's total countries less any credits given for deleted countries. The second number shown represents the total D.X.C.C. credits given, including deleted countries. Where totals are the same, listings will be alphabetical by call sign.

Credits for new members and those whose totals have been amended are also shown.

## PHONE

VK3MS	315/338	VK5AB	298/314
VK3AHO	312/335	VK4PJ	282/301
VK6RU	307/332	VK4TY	275/278
VK4HR	304/322	VK3TL	271/277
VK6MK	304/323	VK3APK	269/274
VK1JZ	303/320	VK2AAK	268/273

New Members:			
Cert. No. 91	VK9WD	106/106	
Cert. No. 92	VK3VK	152/152	

1997

VK4KS 208/203 VK4PX 170/170  
C.W.

9

VK3AHQ	202/306	VK3ARX	201/275
VK3CK	202/313	VK3RU	205/289
VK4PJ	200/313	VK3APK	205/277

AGH	282/296	VKINC	282/296
HR	276/290	VKDCB	276/290

**Amendments:**

BY 1

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## World Admin. Space Radio Communications Conference

Of three resolutions published by the I.T.U., the following extract is worthy of note. Reference is made to this in Federal Comment (this issue).

"... The second resolution, which is no less important, calls for the convening of a World Administrative Space Radio Communications Conference to take place towards the end of 1970 or the beginning of 1971 for a duration of about five weeks.

"The agenda of this conference is to include in particular the following items:

1. To revise existing administrative and technical regulations and adopt such new provisions as necessary for the space radio services and the radio-astronomy services which will ensure the efficient use of the spectrum;
2. To consider, and revise as necessary, the provisions of the Radio Regulations pertaining to the Aeronautical Mobile and the Maritime Mobile Services and to navigation in so far as the use of space techniques is concerned;
3. To consider and provide as far as possible, additional radio frequency allocations for the space radio services;
4. To revise and supplement as appropriate the existing technical criteria for frequency sharing between space and terrestrial systems and establish criteria for sharing between satellite systems.

"In the same resolution, Administrations are invited to submit proposals on the agenda of this Conference. On the basis of these proposals, which will be presented in a report by the Secretary-General, the 24th Session of the Administrative Council will decide on the detailed agenda, date, duration and place of the World Administrative Space Radio Communications Conference."

## VHF SSB

YAESU MUSEN

### FTV-650 Six Metre Transverter

For transmitting, takes low level 28-30 Mc. excitation from an SSB transmitter or transceiver to provide output on the 50-54 Mc. band. For reception, covers 50-54 Mc. with I.F. output on 28-30 Mc.

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## V.H.F. NOTES

Well another year is rapidly growing to a close, the DX activity is on the increase, both on 8 and 2 metres, but alas, no reports of any activity on 432 Mc. Surely there is not the problem of t.v.i. on this band like there is on both 8 and 2 m. Anyway, enough of the moaning, now on to a few brighter subjects.

First, the 1968-69 Ross A. Hull V.h.f. Memorial Contest starts on Saturday, 7th December, 1968, and continues until Sunday, 19th January, 1969.

Secondly, the Festive Season is near, so I would like to wish you all a Very Merry Christmas. Very Prosperous New Year, and may your Xmas stockings be filled with some rare DX. 73, Cyril VK3ZCK

P.S.—Many thanks to those who have contributed to this column over the past year and I hope that you will continue to do so in 1969.

## VICTORIA

Reports indicate that this coming DX season will be one of the best experienced for some years.

Six Metres Band openings which took place in late October enabled all States to work JAs at very good strength. The number of stations using 35-50 Mc. will be interested to know that the VK6s also operate in this band and are anxious to work into VK, while the JAs usually use 50-51.5 with the main activity between 1500 and 2000 E.A.S.T.

Two Metres.—For those who are only on this band these are also looking up, with openings to VK3, J, B, 3 and 7 being quite com. but the occasional opening to VK4 will increase the DX activity on this band.

The VK3 V.h.f. Project Group has almost completed the 3 metre converter, a companion to the very popular 8 metre one which was published in "A.R." about 18 months ago.

Don't forget the Ross A. Hull V.h.f. Contest which starts on 7th December and continues until 19th January, 1969. 73, Robert VK3AUR.

Gippsland.—During the recent CFA exercises much use was made of the 2 m. f.m. channels, with the assistance of a 52.585 Mc.

f.m. link between Thorpdale and Mirroch North and h.f. and s.a.b. On the same week-end David VK3DY, from Maltra, and George VK-3ZCG, from Morwell, attended the V.h.f. Convention at Bendigo. This seemed to start the ball rolling as far as the DX goes, for since then some very good openings have occurred on 2 m. mainly to VK3 and VK7 with a fair sprinkling of the northern VK3s.

## WESTERN AUSTRALIA

The new committee of the West Australian V.h.f. Group are: President, John VK3ZGL; Vice-President, Harry VK3HP; Secretary, Edwin VK3ZAN; Treasurer, Cedric VK3CDT; Committee, Neville Chamberlain, Wayne VK3ZDD and Tom VK3ZAF; Rubeth Editor, Harry VK3HP; Technical Editor, Tom VK3ZAF; Bulletin Circulation, Roy VK3Y, Glen VK3ZFH, Bob VK3ZPV; Broadcast Officers, Kevin VK-62CB/T and Don VK3HK; Oscar Co-ordinator, Don VK3HK; QSL Officer, Laurie VK3ZEA; V.h.f. Records, Rolfo VK3QD; Beacon Officer, Tony VK3ZDT; Press Correspondent, Percy VK3ZDC; Auditors, John VK3TU and Ray VK3KLU.

The club station VK3VF is operated by D. E. Cook, VK3KAW, and runs beacons on 32.696, 15.59 and 432.50 Mc. Another beacon should be in operation by the time these pages are being read. This is at Albany and will be on 144.5 Mc. with a beam on Adelaide and another on Perth. The power is about 60w. to a converted Fye base station and is sited on a 1,500 foot hill with a good path to the East.

Nois used in this State are 32.585, 32.693, 52.8 and 52.820 Mc., all a.m., plus 32.585 and 144.50 Mc., both f.m. 73, Percy VK3ZDC/T.

## NORTHERN TERRITORY

Activity from the Darwin area should be much greater this year, now that active Amateurs include Doug VK3ZG, Jim ex VK3ZJ and myself (Bruce VK3AZ, ex VK3AZG). We are working on a Radio Booster Station at Cox Peninsula for Radio Australia. I hope to establish regular schedules on 30 and 40 metres with either VK3BA or VK3VO and possibly with VK3AZK, with all of whom I used to work. 73, Bruce VK3AZ.

## NATIONAL FIELD DAY

The John Moyle Memorial National Field Day Contest, 1969, will be held from 0900 G.M.T., 1st February, 1969, to 0800 G.M.T., 2nd February, 1969.

The rules for this contest will be published in the next issue of "A.R."

## STATE INTRUDER WATCH CO-ORDINATORS

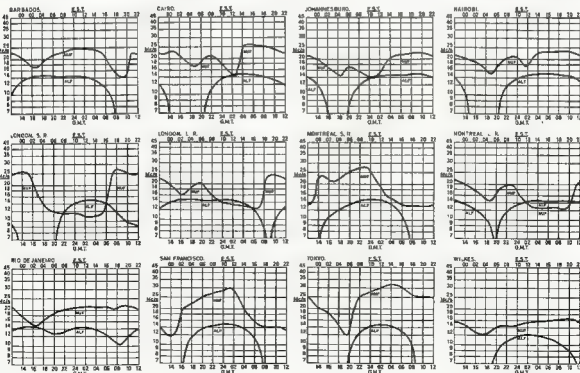
New South Wales—  
W. H. R. Treloar, VK3HPZ, 33/8 Fullerton St., Woolahra, N.S.W., 2025.  
Victoria—  
M. P. Davis, VK3ANG, 144 Tramway Pde., Beaumaris, Vic., 3193.  
Queensland—  
Cec. Kenny, 19 Lithgow St., Wynnum North, Qld., 4178.  
South Australia—  
W. J. Bulling, VK3KK, 297 Goodwood St., Kings Park, S.A., 2034.  
Western Australia—  
G. Allen, 253 Amelia St., Balga, W.A., 0601.  
Tasmania—  
D. H. Kelly, VK3DK, 56 Upper Brougham St., Launceston, Tas., 7250.

## CONTEST CALENDAR

Until 31st Dec.: Concurso Mexico 1968 (I.S.R.E.).  
7th Dec., 1968, to 15th Jan., 1969: Ross A. Hull V.h.f. Contest (I.S.A.).  
1st and 2nd Feb., 1969: John Moyle Memorial National Field Day (W.I.A.).  
1st and 2nd Feb., 1969: 35th A.R.L. DX Test (Phone Section), first week-end.  
1st and 16th Feb., 1969: A.R.L. Novice Round-up (C.W. Section), first week-end.  
15th and 16th Feb., 1969: 35th A.R.L. DX Test (Phone Section), second week-end.  
8th and 9th Mar.: 35th B.E.R.U. Contest (I.S.G.B.).

## PREDICTION CHARTS FOR DECEMBER 1968

(Prediction Charts by courtesy of Ionospheric Prediction Service)





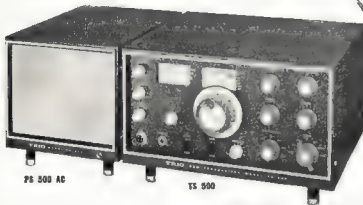




# TRIO

## SSB transceiver

200 watts PEP—7 Bands—A M & C W  
and  
Power Supply and Speaker Unit



PS 500 AC

TS 500

### SPECIFICATIONS

Frequency:	80m Band	3.5-4.0 MHz
	40m Band	7.0-7.5 MHz
	20m Band	14.0-14.6 MHz
	15m Band	21.0-21.6 MHz
	10m A Band	28.0-28.6 MHz
	10m B Band	28.5-29.1 MHz
	10m C Band	29.1-29.7 MHz

Communication Methods: SSB (A3J)  
AM (A 3H)  
CW (A1)

Maximum Input Power: (Xmitter final stage)  
200W (PEP)

Standard Input Power: (Xmitter final stage)  
180W (PEP) 120W on 28 MHz band only

Antenna Input Impedance: 50-75 ohm

Carrier Suppression Ratio: More than 40 dB

Single Side Band Ratio: More than 40 dB

Mic. Input Impedance: High Impedance  
(dynamic or crystal mic. recommended)

Xmitter Audio Frequency Characteristics:  
300-3,000 Hz (-6 dB)

Receiver Sensitivity: 1µV S/N 10 dB  
(1.4 MHz)

Receiver Selectivity: 2.7 kHz (-6 dB)  
5.0 kHz (-55 dB)

Spurious Rejection Ratio: More than 45 dB

Image Ratio: More than 60 dB

Undistorted Power Output: More than 1W

Receiver Output Impedance:

PS 500 ohm

PHONE 8 ohm

Power Consumption (using PS-500AC):  
450W (At maximum power output)  
250W (Receiving Mode)

Tubes and Transistors used:

17 TUBES, 3 TRANSISTORS, 15 DIODES

Dimensions: W: 13 1/2"; H: 8 1/2"; D: 11 1/2"

Weight: 17.6 lb

FOR/FOA SYDNEY: TS 500, \$491.00; PS 500 AC, \$96.00

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## V.H.F. U.H.F.

Interested in what European Amateurs are accomplishing on these bands. Commencing January 1969, the authoritative German v.h.f. u.h.f. magazine UKW-Berichte will be published quarterly in English. 60 pages of the latest techniques, detailed construction articles on v.h.f. u.h.f. gear and antenna written by top Amateurs in Europe.

Annual subscription \$5.50 AIR MAILED direct from the German publishers. Send a cheque/money order to the Australasian representative of UKW-Berichte, G. Clarke, VK-2ZXD, 2 Beaconsview St., Balgowlah, N.S.W., 2093.

A LIMITED number of sample copies of the German edition are available free for inspection.

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- \* Model 55 Swantenna five-band Mobile remote control Whip Antenna, \$190.
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## **Changes for Mobile Radiotelephone Services**

Licencees of V.H.F. land and harbour mobile radiotelephone services, now operating in 30 kc/s channelling areas, are advised that if they have not already installed equipment which meets the Australian Post Office 30 kc/s channelling specification, they must do so before 30 June, 1969.

This requirement has been brought about by the growing demand for V.H.F. mobile radiotelephone services in city areas which is taxing the existing channels available. The change to 30 kc/s channelling will enable more radiotelephone services to be brought into operation as they are required.

However, some changes to existing equipment will be necessary and the following programme for conversion, which is designed to cause the least inconvenience to all concerned, has been adopted:—

As from 30 June, 1969, licencees of V.H.F. mobile radiotelephone services operating in 30 kc/s channelling areas within the frequency bands 70-85 Mc/s and 156-174 Mc/s\* will be required to make necessary changes so that:—

- (i) All base station transmitter/receivers (both amplitude and angle modulated) employed in a base station installation shall be of a type complying with the relative Post Office specification and approved for 30 kc/s operation and shall be operated in accordance with the terms of that specification.
- (ii) All angle modulated mobile transmitters shall be adjusted to function with a maximum deviation of  $\pm 5$  kc/s.

\* This excludes the International Maritime Mobile V.H.F. Radiotelephone and the existing Australian Post Office Subscriber Services.

Early conversion will assist manufacturers in meeting delivery dates for equipment.

**FURTHER DETAILS MAY BE OBTAINED FROM THE SUPERINTENDENT,  
RADIO BRANCH, G.P.O., IN YOUR CAPITAL CITY.**

**AUSTRALIAN POST OFFICE**

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